



Optimizing The Maximum Power of Photovoltaic System Using Modified Incremental Conductance Algorithm Operating Under Varying Dynamic Climatic Conditions

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Received 8 Apr. 2023, Revised 8 Jan. 2024, Accepted 21 Jan. 2024, Published 1 Feb. 2024

Abstract: In a photovoltaic system the challenge is to contentiously searching for the maximum power point to generate the maximum power (Pmax) within the system. In this study a hybrid maximum power point tracking module (MPPT) consisting of a well-known incremental conductance algorithm (INC) is being adapted to operate along with fuzzy logic controller (FLC). The new design focused on applying variable voltage step size estimations based on analyzing the degree of incremental and decremental of power to voltage relation. To achieve this, five effective regions were introduced around the maximum PV power point and FLC controlled the tuning and accurate adjustments of the duty ratio cycle step size by relying on the inputs of fuzzy logic controller to reach a zero oscillation around the MPP point. To adjust the duty cycle step size, fuzzy logic is established based on the position of the fuzzy input points which are derived from the current and voltage proportions and their derivatives, whereas the membership functions and rules are shaped. Matlab simulations were used under different irradiance levels to test the efficiency of tracking the maximum power. Based on the simulated results, the integration of fuzzy logic controller with incremental conductance algorithm provided enhanced performance in tracking the Pmax, and notable fast convergence time and provided the least oscillation around the maximum power point and thus maintained the overall tracking accuracy, and applying the proper step size to drive the operating point at the P-V curve in reaching Pmax under the effects of various environmental dynamic changes in temperature and irradiance.

Keywords: Incremental conductance, Fuzzy logic, Adaptive step size, PV system, Intelligent control system, dc-dc converter

1. INTRODUCTION

Solar energy is getting more popular and of interest at the level of renewable energy source category because photovoltaic (PV) modules and systems have low maintenance costs, and quiet in terms of the noise and can range in size from large kilo-watts to very few milli-watts allowing for efficient integration into our current environment [1],[2],[3]. As a result, the PV energy's amounts generated and produced are rising and getting a noteworthy part for both the industrial and domestic subdivisions.

In fact, the limitation to the spreading of PV power systems comes to many reasons however not to count the cost only, but the in-ability of PV cells in transforming/converting the energy of solar radiation into electrical power. Currently, conversion in the energy and its efficiency is close by and about twenty percent, assuming that the solar cells are working at their maximum rate [4], [5].

PV cell output power (Pout) to its operating voltage has the

characteristics of a non-linear function with respect to each other's. Such an identified function has an MPP equivalent to a certain voltage value; similarly, the PV array performance would rely on different other factors such as voltage operation, shading, irradiance and temperature [6], [7].

The main goal sought in PV solar panels and systems is to track and reach the MPP. To achieve this goal, an extra module shall be implemented. This would be achieved through a power converter [8], [9]. The converter shall be connected to the PV output's module; this inverter drives the PV module output voltage to reach the optimal value considering the aforementioned atmospheric conditions and their versatilities that affect the overall performance of the system.

In the most recent years, many approaches were addressed to reveal their capability of controlling converters while looking to address tracking the MPP through applying different MPPT algorithmic methods

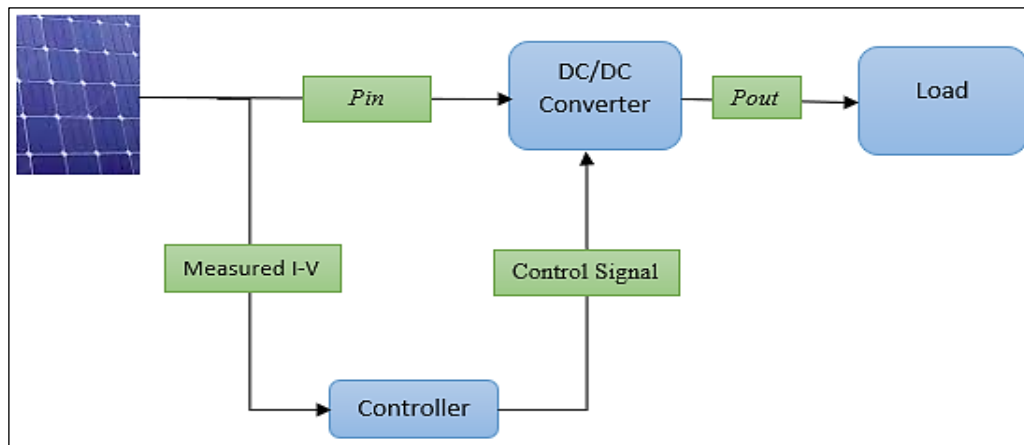


Figure 1. MPPT block diagram

[10]. Those are currently recommended and their assessment is presented in several set of articles. The main block diagram of MPPT is shown in Figure 1 [11].

In fact, two well know algorithms have been studied by many researchers in regards of tracking and extracting the MPP and those are the Perturb and Observe (P&O) as well as the Incremental Conductance (INC) methods [12], [13].

Numerous MPPT systems have been addressed as per the literature. Along of that some techniques are uncomplicated, relying on voltage/current feedback. However, they necessitate sporadic interruption of the PV modules for measuring the V_{oc} or the I_{sc} for reference, leading to increased losses in power (Liu et al).

The (P&O) algorithm (Abdul et al), hill climbing (HC) and incremental conductance (IC) algorithms (Kiesh et al.) are more improved in tracking the MPP however they require more complicated settings. The incremental conductance algorithm works on the principle of applying at the PV's module operating voltage a perturbation. The HC algorithm applies a perturbation at the DC-DC converter's duty cycle which makes it more favorable since its control structure is simple to adapt (Alaj et al.).

The development of MPPT controllers utilizing neural network and FLC techniques resulted in faster tracking speed of the MPP and more accurate performance in extracting the P_{max} of a PV system (B. Salh and Oali et al.). In particular, FLC have demonstrated superior performance compared to other control methods, and are able to maintain good performance even under varying atmospheric conditions (Isram et al.).

Most of the well know algorithms and precisely the INC, relies on a fixed step size perturbation when applied in a direct control. However, this conventional practice has

several disadvantages, that can be listed as follow; the convergence speed is very slow in reaching the operating point at the optimal level and this is due to the fact that the fixed step size perturbation is applied [14], [15]. Further in the steady state, the oscillation of the driven operating point to reach the MPP or around it using a conventional INC algorithm leads to a major loss in energy (overall extracted power) [16]. In addition, INC algorithm cannot track the MPP at severe climatic conditions due to the use of pre-determined and fixed step size perturbation [17], [18].

The operating voltage of PV system relies on MPP location to keep updating it by tuning and changing the power converter duty ration cycle through a series of fixed step sizes [19], [20]. In the past studies of the most recent tracking algorithms, it has been well known that the P&O is easier to implement when compared to an INC method. However, it degrades from its lower accuracy results when tracking the MPP, regardless of the testing environmental conditions whether being constant or non-constant [21], [22]. On the other hand, the INC method can provide better accuracy as compared to the P&O algorithm however for the price of being more complex mechanism and slower convergence time. Such complexity is capable of providing an ultimate and reasonable performance for rapid changes in atmospheric conditions [23], [24], [25], [26].

The curve of the current-to-voltage (I-V) and its characteristics under the normal test conditions is depicted in Figure 2. This curve denotes a particular characteristic of a PV array. It provides a description of the conversion in the solar energy efficiency [27], [28]. Once the I-V characteristics for solar cell is known it will be essential in the determination of the efficiency of solar system and the PV overall output performance [29], [30], [31].

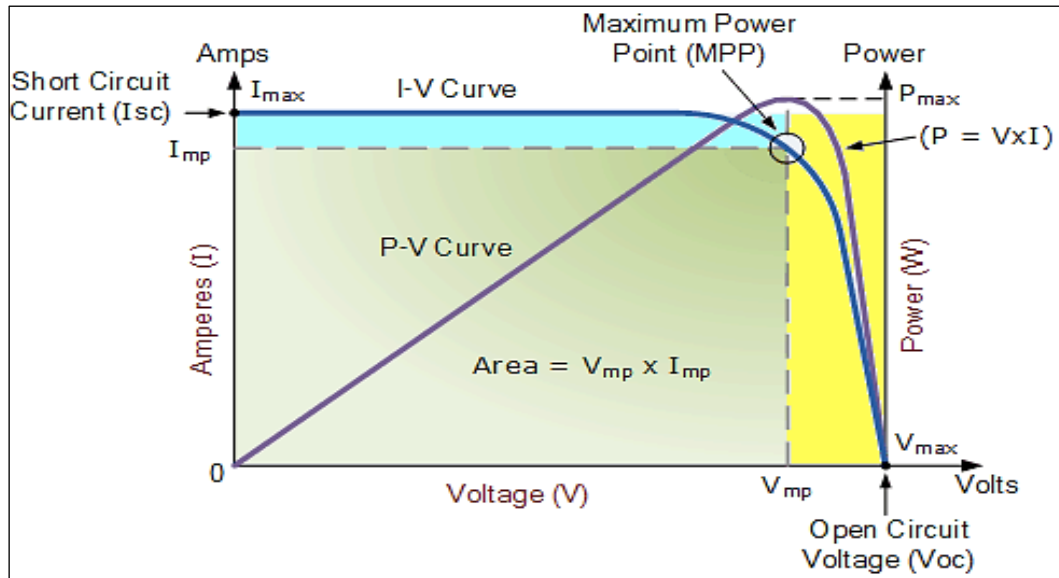


Figure 2. General characteristic current-voltage curve

At the stage of the open-circuit state, the voltage (V_{oc}) is obtained through the maximum voltage (V_{max}) and vice versa, the (I_{max}) is being attained through the short circuit state (I_{sc}).

A PV array operational point is lying always between the above mentioned two states, denoted by $(0, V_{oc})$ and $(I_{sc}, 0)$. The combinational product of both the current and voltage is going to be at the maximum. Hence, that point is normally denoted as the maximum power point (MPP).

Once we refer to the MPP, the current and voltage are represented by $(V_{mp}$ and $I_{mp})$. As per solar panels, when we operate them at the operating points that are not guided or directed to reach the MPP, then the power extraction from that PV module will be degraded and hindered in extracting the maximum power [32], [33].

The PV system operating point is found on the characteristic curve and its location is not constant due to the changes associated with the irradiance and temperature at certain given time period. To harvest the P_{max} at different temperature levels and irradiances, the operating point of the system must reach the maximum peak of the P-V curve. Once this condition is satisfied, that point is called the maximum power point denoted as (MPP). To extract this MPP out of the module it will be essential to drive the current operating point to operate at the peak level of the MPP of the P-V curve [34], [35].

Along this research we will implement a type of hybrid MPPT consisting of two schemes: incremental conductance control (INC) and novel fuzzy logic (FLC) control. This approach seeks and tracks the maximum power point (MPP) under a different set of dynamic solar irradiances. Additionally, it will precisely adjust the duty ratio cycle of a DC-DC converter to speed up the tracking process of MPP [36]. Simulation analyzes are performed to test the tracking accuracy and overall performance of the suggested approach in this research study. The obtained testing simulations and results were promising in regards to the tracking scheme of MPPs under varying

irradiances and diminished the oscillation around the maximum power point of the PV non-linear curve [37], [38].

For this proposed work, a photovoltaic system is used, which consists of many interconnected photovoltaic sets of cells and apply a conversion from sunlight form to an electricity form. The load impedance will determine both the current and voltage through which PV module operates [39], [40].

To recap, in this research a proposed modified INC variable step size perturbation based FLC controller is implemented to overcome the degradations of power losses of the conventional fixed step size technique, where the adaptation of variable step using an FLC intelligent controller provided the following positive outcomes based on the simulation results [41], [42], [43]. The below points were addressed, investigated and tested through the course of investigating the proposed system [44], [45], [46];

(1) The PV operational conditions are subject to changes due to the changes of temperature and irradiance. To address these variations effectively, FLC was employed in this research study to adjust the step size in the INC algorithm dynamically, enabling real-time adaptation to the evolving conditions. (2) Utilization of variable step sizes based on fuzzy logic improved the overall MPPT efficiency as demonstrated in the simulation results there were obtained from Matlab Simulink. (3) INC based on FLC intelligent control was able to adjust the step sizes based on the changes of the systems' dynamic weather parameters that minimized the oscillation factor around the MPP, permitted the system to converge more faster at the MPP level, and demonstrated a major reduction in the response time of driving the operating point on the P-V curve towards the optimal MPP [47], [48]. (4) Applying FLC provided the advantage of operating and making decisions simultaneously based on different sets of changing input parameters (i.e., the current and voltage) and this was revealed through the set of pre-defined FLC rules to

generate the optimal output power of the designed PV system [49], [50].

2. CHARACTERISTICS OF I-V AND P-V CURVE

To gain an enrich insight of the operational and performance as we address solar panels, it is essential to examine the characteristics perspective of both the I-V and P-V curves in a photovoltaic environment [51], [52].

Those curves are needed to assist in detecting the degradation level and the sort of low performance causing a solar panel to function under its expected output level [53], [54], [55].

Figures 3 and 4 demonstrating the I-V and P-V respectively, with a different range of irradiance values and temperature [56], [57]. As per Figure 3, an I-V nonlinear curve is shown with different ranges of irradiances. Normally this curve represents in a graphical means the solar array's operation and therefore addressing the current and voltage relationship at a set of irradiance level value [58], [59], [60], [61].

Climate factors, like temperature and irradiance, have a direct impact on the I-V curve of a PV module, leading to deviations in its maximum power point (MPP) [62], [63]. Considering that, practical PV systems operate in

dynamic conditions where these factors are continuously fluctuating, it becomes essential to continuously adjust the operating point of the PV module to match the new MPP [64], [65].

This curve gives the necessary information during the configuration of a PV system to make it operating at the optimal maximum power point (MPP). In addition, this curve depends on the quantity of irradiance hitting the solar panel modules [66], [67].

When an increase in irradiance (during peak hours of the day) takes place, this will lead to increase the current at the vertical axis as shown in Figure 3. For instance, when the irradiance increases from 400w/m^2 to 1000w/m^2 we observe that the effect of irradiance on the short circuit current (I_{sc}) is linear and thus it increases linearly and proportionally with the solar irradiance level [68].

As per the effects of the open circuit voltage (V_{oc}), when the irradiance increases the V_{oc} will also increase. However, in this scheme the V_{oc} is ranging between 1.3 and 1.5 volts (due to irradiance changes) and thus the solar irradiance effects on the V_{oc} are not that significant [69], [70].

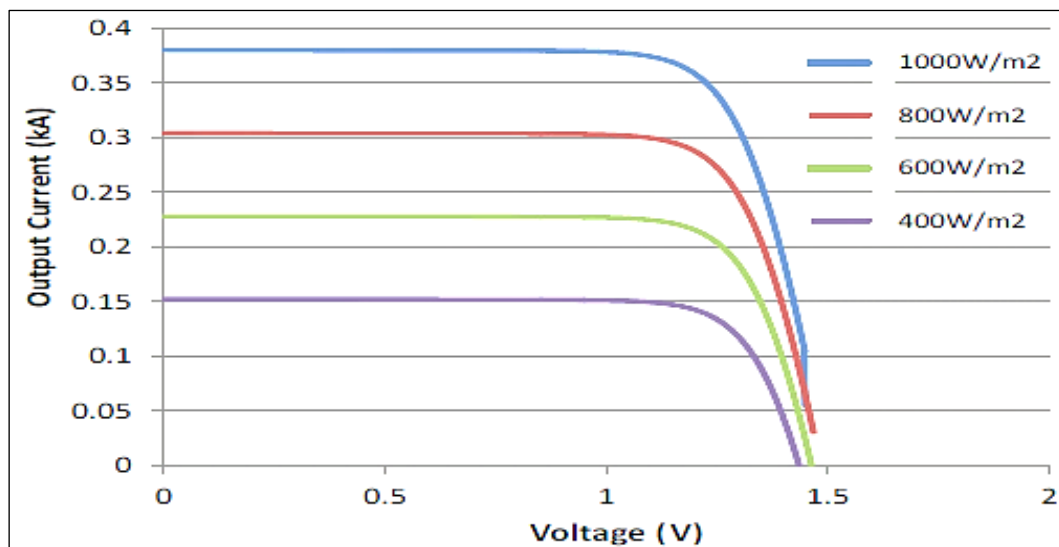


Figure 3. PV module I-V curve for various irradiances

As per Figure 4, it represents a PV solar panel with a 60W power efficiency. The P-V curve is analyzed under varying temperature levels [71], [72]. It is noted that the temperature and power are inversely proportional in this scheme where the power will decrease when an increase in temperature occurs [73], [74].

In fact, both the output power and voltage of the solar array is decreasing when the operating temperature of the solar cell is increasing [75].

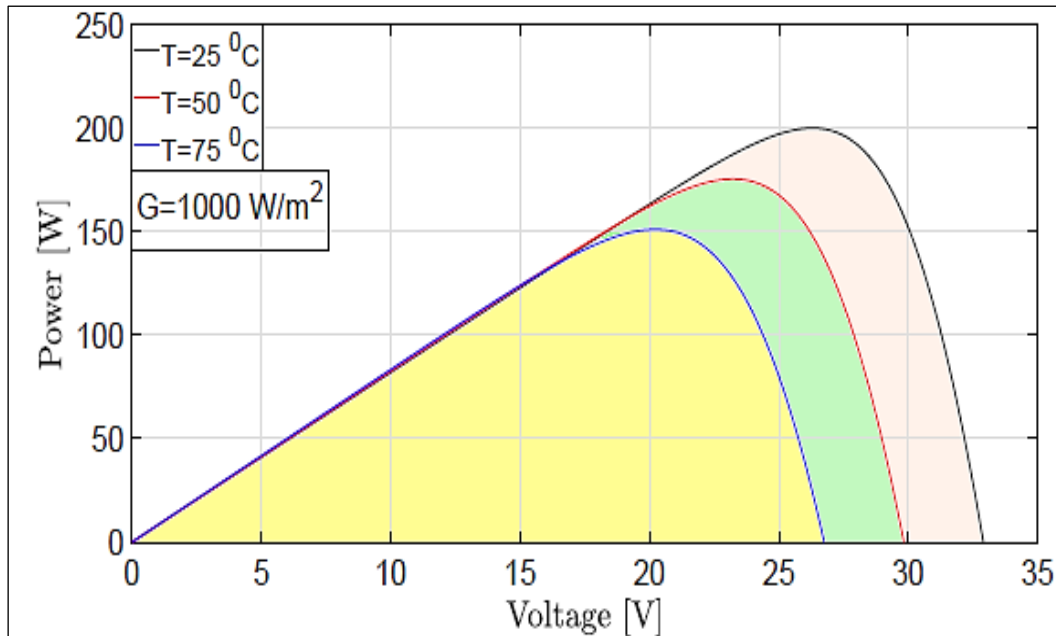


Figure 4. P-V characteristics curve with varying temperatures

From the above illustrations we notice that many parameters affect a PV array which reveals a non-linear characteristic in term of either I-V or P-V curves whether there was a change in irradiance levels or temperature values. This will lead to loss of the system's energy and eventually degradation in tracking the maximum power point (Pmax) of the PV system. To overcome this optimal power loss and to affirm PV solar arrays are operating at the Pmax under the above versatile parameters' conditions, a maximum power point track mechanism is crucial to be incorporated. It diminishes the oscillations around the Pmax on the P-V curve and maximize the overall energy of the system [76].

To summarize, the efficiency of photovoltaic systems is typically affected by climatic conditions, including solar radiation denoted as (G or S) and temperature (T).

3. MPPT TRACKING THROUGH THE IMPLEMENTATION OF INCREMENTAL CONDUCTANCE ALGORITHM

MPPT is an algorithm utilized to enhance the efficiency of a PV module. Multiple MPPT systems are designed to seek and track the MPP. In general, a decent and reliable range of such algorithms are available to line-up the PV module to operate at the full power extraction point MPP [77].

In general, we have a variety of different types of MPPT algorithms. The most well-known for instance, would be the perturb and Observe(P&O) and the incremental inductance (INC). These algorithms used to tack the MPP, and can be integrated with different variety of controllers, such as, fuzzy logic controller (FLC) [78].

The P&O algorithm, operates in the sense of perturbing the voltage and observing the power in a path of keep monitoring and driving the operating point (current direction) to move it towards the MPP and reaching it.

Technically speaking, the P&O continuously has a role of targeting the current location of the operating point and move it to the desired location on the P-V curve [79].

Consequently, and back to the PV module, when the operating point moves away and not aligning with the MPP, the voltage will be perturbed (adjusted) in the reverse direction. Many researchers addressed the P&O in their research papers, along with the Hill Climbing (HC).

The above mechanisms and approaches, unfortunately, will have a negative impact due to causing the operating point on the P-V curve fluctuating around the MPP. This oscillation around the MPP is normally due to environmental climatic conditions that changes drastically, as well as, when the load is changing.

The incremental conductance (INC), operates in another and different way as compared to P&O, where (INC) function and operates through a special and unique mechanism. It concentrates on the PV power slope rather than the voltage curve. Through this functionality approach, it's capable to optimize reaching the ultimate and most desired MPP at zero (This is the location where the maximum power extraction occurs).

INC has a special characteristic where it utilizes a fixed iteration step size. Dealing with fixed iteration step size has proved to have many performances limitation according to many researches when it was used in tracking the MPP [80].

Our proposed approach deals with integrating the INC algorithm along with one of the most known controllers, the fuzzy logic control (FLC).

The direction of this study in this paper is to work on reducing the shortcomings of the conventional INC algorithm. In addition, the anticipated module is designed to minimize and reduce the oscillation that is taking place and re-occurring around the MPP.

Furthermore, another achievement of the proposed hybrid tracker to improve the steady-state performance as well.

In addition, through this investigated theme, we recommend an improved INC algorithm established on the approach of utilizing a variable step size versus the fixed step control where the variable step size improves both dynamic (sudden irradiance fluctuations) and stability of the overall functionality and the system's performance of the photovoltaic module during extracting the Pmax [81].

4. IMPLEMENTATION OF MPPT ALGORITHM USING INCREMENTAL CONDUCTANCE

As one of the most popular algorithms in tracking the MPP, the incremental conductance (INC) would serve its purpose as an MPPT algorithm. It depends on the most important two parameters in a photovoltaic system, namely the PV voltage and current. The maximum power point tracking (MPPT) has enhanced the overall performance of a PV module especially under dynamic climatic changes. The INC as compared to P&O has overcome the optimization to the PV system.

In an incremental conductance, the method used to find and track the MPP is relying on comparing the incremental conductance to the instantaneous conductance. Since the MPP is determined when the change of power to voltage ($\Delta P/\Delta V$) is set to zero; using the product/chain rules we can deduce the following [82];

$$\frac{dp}{dv} = \frac{d}{dV}(VI) = 1 + \frac{VdI}{dV} = 0 \quad (1)$$

Applying the method of approximating to the (dI/dV) through selecting small step size with a small value, then

we may assume that the $\Delta I/\Delta V \approx dI/dV$, and this would lead to get:

$$\frac{\Delta I}{\Delta V} = -\frac{I}{V} \quad (2)$$

This in conclusion would stress that the operating point is at MPP under the condition when the incremental conductance is approximated as the conductance of the instantaneous conductiveness. In the same manner, when the incremental conductance is falling smaller than the instantaneous conductance; hence in such state, the operating point shifts to the left of MPP; i.e., operating voltage must increase and vice versa.

To work on reaching the MPP, stated in equation (1), INC algorithm apply a searching operation in tracking that point through accessing and applying a control structure of the (V_{ref}) to duty cycle (D), knowing that V_{ref} is the reference voltage in this case.

When the MPP state is not satisfied, INC exerts continuous searching to satisfying that state. Knowing that MPP state is reached as the left side (1) is equal to zero. Consequently, when left side (1) > zero, in this case V_{ref} increases.

When the left side (1) is < zero, V_{ref} decreases. This situation is designated in Figure 5, where the left side shows that the instantaneous conductance and the incremental conductivity summation are greater than zero [83].

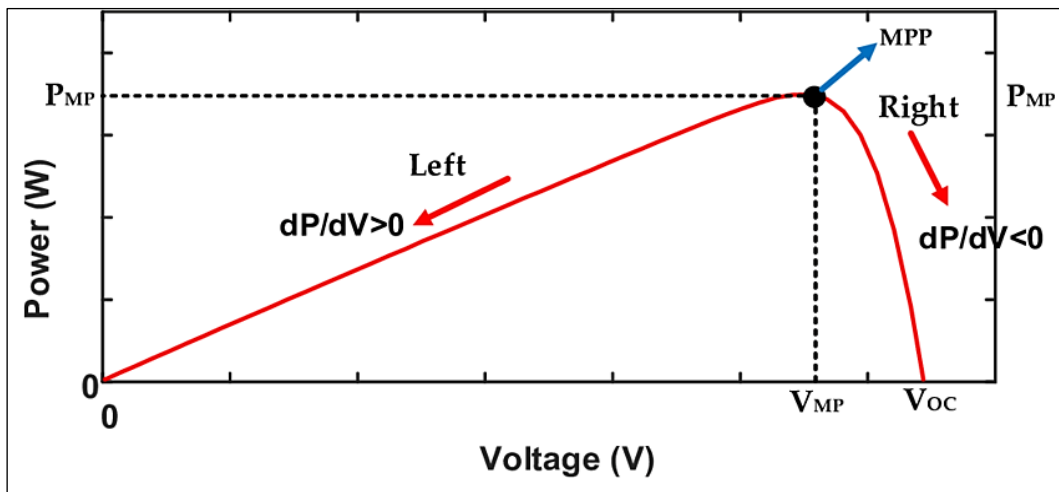


Figure 5. Operating MPP point location on P-V curve

On the contrary, and as we discuss the other side which is the right section of the curve, it reveals that the instantaneous conductance and the incremental conductivity summation is < zero.

In Figure 6 INC flowchart operation is being exhibited. Normally, the control signal output of INC algorithm

works on the adjustment of the photovoltaic V_{ref} . This is achieved by the increase and decrease of the constant value denoted as (ΔV) to the prior reference voltage. Note that in this mechanism the tracking is done through a series of fixed step size regardless of the operating point location versus its optimal power point Pmax on the P-V curve.

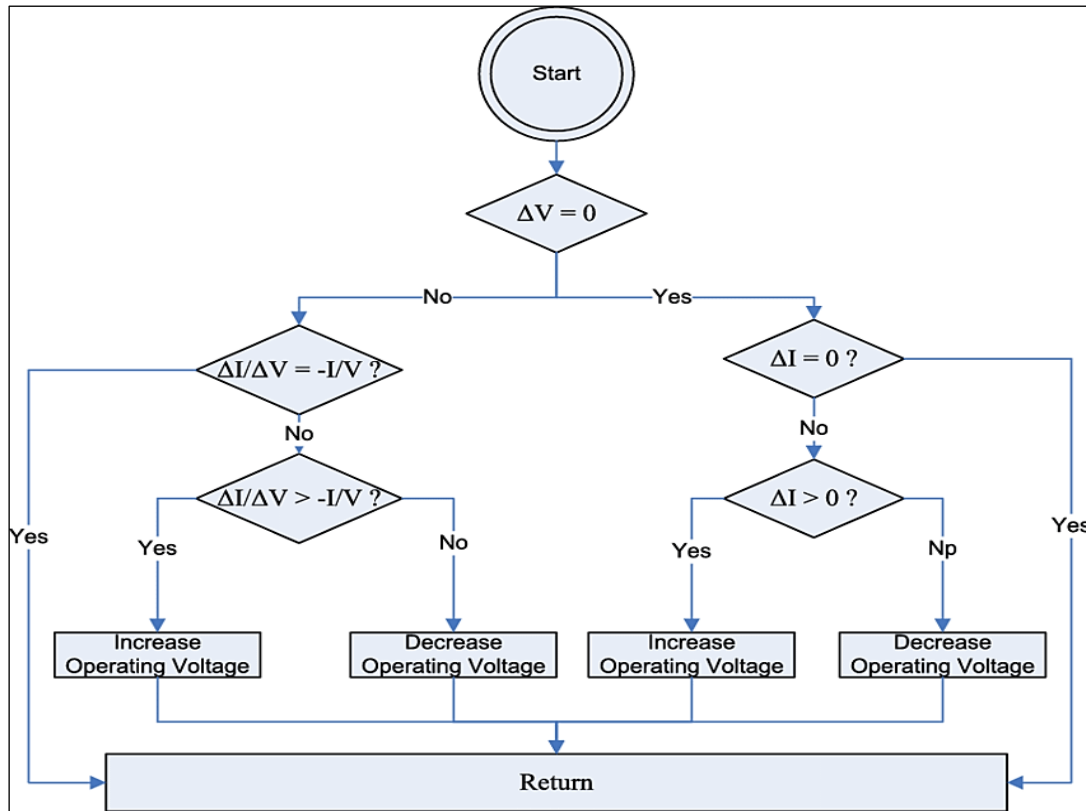


Figure 6. Incremental conductance operational flowchart

Reaching the $\frac{dP}{dV} = 0$ slope is not a normal reached case. To align and track the non-zero slope, we need to get a minimal marginal error, and that error's value will rely on the requisite sensitivity of MPPT. This error can be determined through the following equation [84].

$$e = \frac{dI}{dV} + \frac{I}{V} \quad (3)$$

Three cases are noted in regards to the error at three different stages;

- Case 1: when the error is greater than zero ($e > 0$); Here operating point to the left of the maximum power point (MPP)
- Case 2: when the error is equal to zero ($e = 0$); Ultimate extraction of power at this stage where the operating point is at MPP
- Case 3: when the error is less than zero ($e < 0$); In this scenario we conclude the operating point is located at the right of MPP.

To summarize, in the below table it shows the three cases as seen from the incremental conductance perspective.

Table 1 is drafting the three cases of detecting our best location for the maximum power point (MPP).

Table1. The INC three cases of tracking MPP

Right [of MPP]	$(d_p/d_v) < 0$	$(\Delta I/\Delta V) < -I/V$
At [MPP]	$(d_p/d_v) = 0$	$(\Delta I/\Delta V) = -I/V$
Left [of MPP]	$(d_p/d_v) > 0$	$(\Delta I/\Delta V) > -I/V$

Having revealed some strengths of the INC algorithm however, it has a definite disadvantage: The need and requirement to perform excessive and additional more complex calculations, as well as it has a negative drawback in consuming the memory of the system.

5. VARIABLE STEP SIZING PROPOSED FLC CONTROL FOR MPPT ALGORITHM

With an applied incremental conductance (IC) algorithm and during a change in the solar irradiance level from lower to higher level, the traditional incremental conductance algorithm would inaccurately respond in the first step size changing at the converter duty cycle.

However, with the new modified incremental conductance algorithm it can deliver a more precise values as the level of solar irradiance increases. This will lead to provide a zero oscillation at MPP that eventually allow a full extraction of power from the PV module. [85].

Fuzzy logic controller (FLC) considered as a branch of intelligent controllers. FLC theory is attained by imitation and acquisition of human behavior. In addition, FLC never depends on a complex mathematical model calculations as other controllers would require; however, it deals with imprecise input and this drive the authors of this research to implement it in extracting the Pmax of PV system.

Although the literature has discussed various methods for tracking the operational optimal point, however, the utilization of artificial intelligence, specifically fuzzy logic, has been selected to enhance the performance of the controller to achieve the maximum power point. This is conducted through a set of MATLAB SIMULINK simulations and a design modeling of FLC based MPPT control system [86].

FLC methodology design is based on the nonlinearity of the PV system comprises the following components as shown in Figure 7A.

FLC essentially includes, three different processes through a fuzzification process, knowledge base (inference rules) and defuzzification process. This is depicted in Figure 7B and Figure 7C.

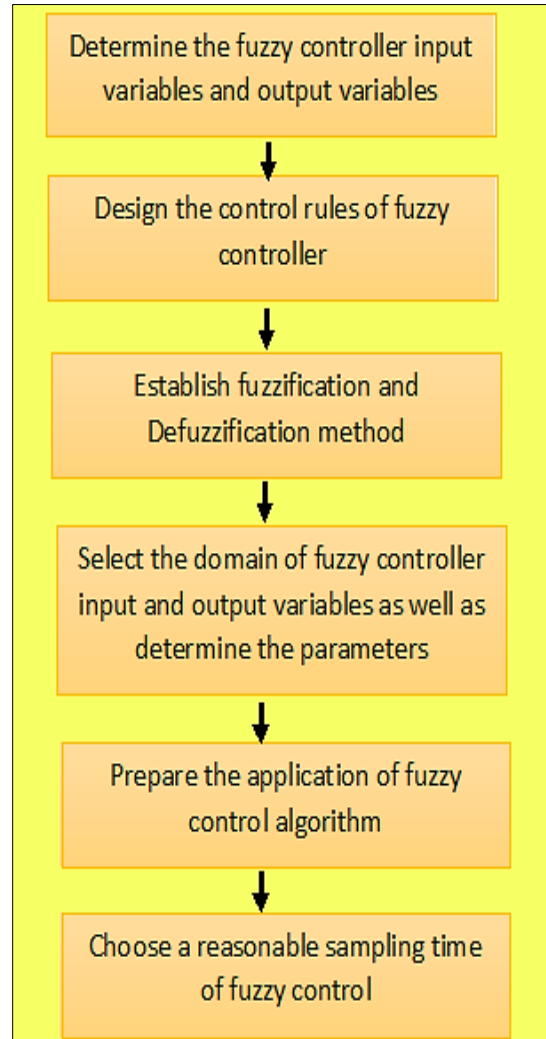


Figure 7A. Methodology of FLC design

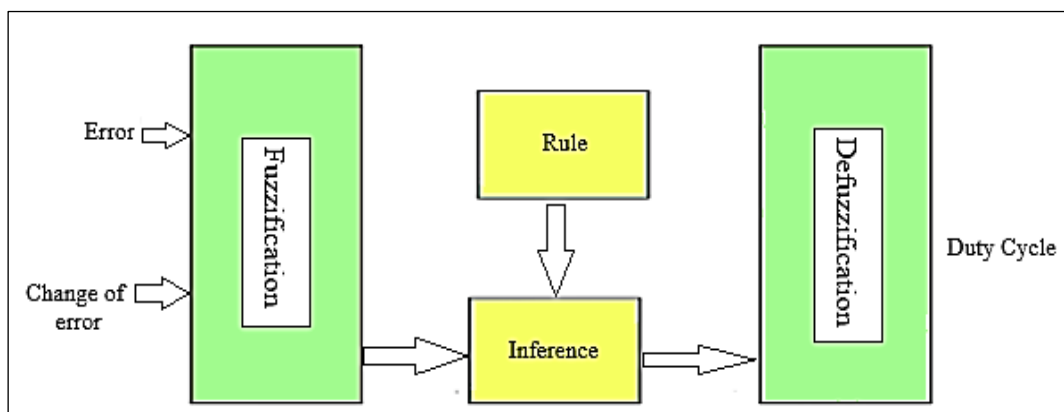


Figure 7B. Block diagram of fuzzy logic controller

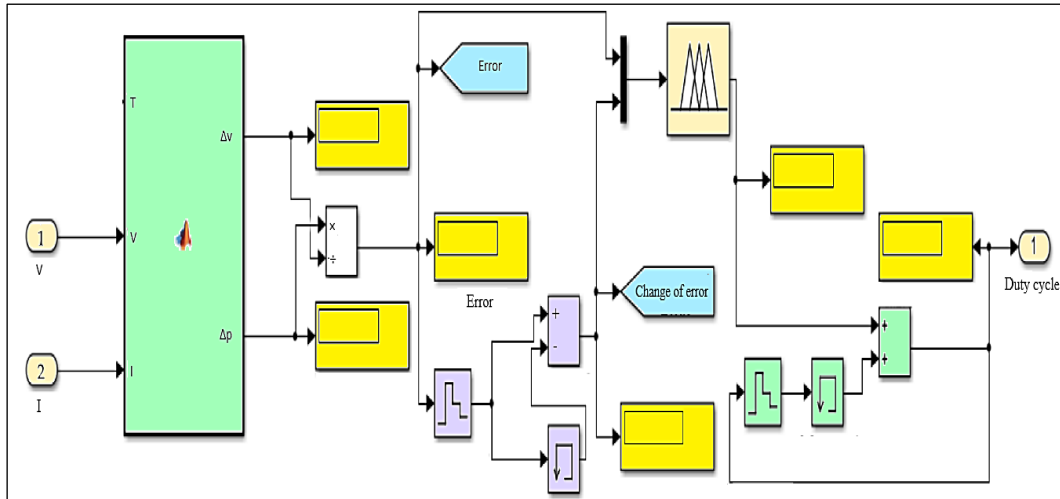


Figure 7C. Block diagram of Matlab FLC circuit

At the fuzzification process the numerical input variable of the change of power to the change of voltage is converted to a crisp values represented by a set of membership functions.

Such a controller has been configured to have two inputs and one output. The two inputs are the error (E) and the change of error (CE). Note that, these variables are fed for processing purposes, to an inner inference system and a set of rules [87].

These conditions are implemented to generate the fuzzy logic output. The last process in the fuzzy logic control is the process of defuzzification.

At this stage the output is denoted by the fuzzy duty cycle ratio change (ΔD). During the defuzzification process, crisp value will be set back to the original state which is converted back to a numerical value and fed in the photovoltaic system.

In Figure7D, the algorithm of the INC based FLC measures how far the distance of the current operating point from the MPP and based on the current step size the adjustment of ΔV is applied to improve the response time in regards to tracking the MPP and this is achieved through the implementation of FLC. In addition, the direction of the operating point on the P-V curve is determined during that process (either to the right or left of the curve).

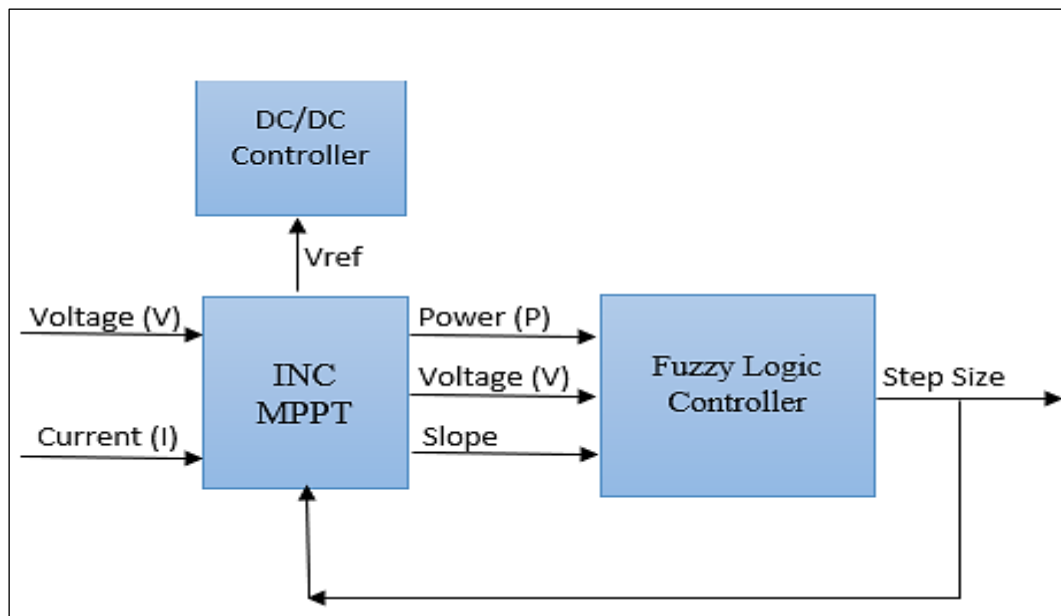


Figure 7D. FLC integration in ΔV step size

The distance of the current operating point is governed through the slope calculations of the current PV operating point.

When the operating point is closely approaching the MPP, the slope derives a small step value size and vice versa for an operating point that is far away from the MPP point.

In the next discussions we will address the applied membership functions of the two inputs and one output. Those MF functions are created using linguistic variable such as “Negative big”, “negative small”, “zero”, “positive big”, “positive small”, etc.

The FLC control consists of five membership function (MF) at every individual input of the universe of discourse. This would generate through the controller a set of 25 rules. Knowing that FLC depends on these rules to initiate the control of the PV system in term of adjusting the step sizes of the operating point during the tracking and seeking of the optimal MPP [88].

In FLC a collection of rules that govern the relationship between its input variables against its output actions. The rules in an FLC's rule base generally follow an "if-then" structure and employ linguistic variables to define the system's behavior.

The formation of these rules is dependent on an expert knowledge or experiential observations to drive the decision-making process of the controller.

As per this research the fuzzy rules are applied to minimize the system's error and reach what's called “zero error state” through the maximum power point (MPP) steady state. Further those 25 rules are forcing through the FLC controller the operating point of the PV system to move towards the MPP [89].

This is achieved by adjusting the duty ratio cycle (increasing or decreasing) based on the current location of the operating point and its position from reaching MPP.

As a result, when the operating point is at a very close by distance from MPP, then a smaller step size needs to be applied and the duty cycle will be decreased or increased slightly and vice versa when the operating point is far away from the MPP where the duty cycle will be decreased or increased in a larger scale to reach MPP.

In Figure 8 the FLC based MPPT tracking algorithm is introduced. This block structure consists of two inputs denoted as the error (E), the change of error (CE), and an output representing the change of duty cycle (ΔD) [90].

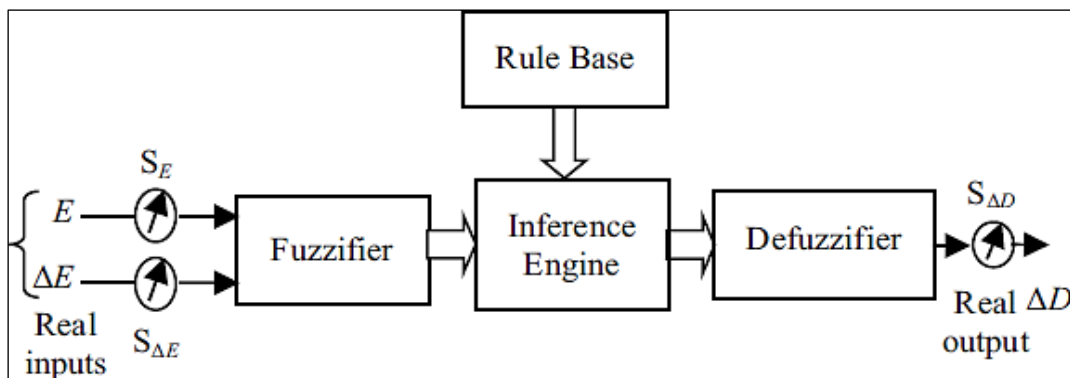


Figure 8. FLC controller with 2 inputs and 1 output

The above-mentioned two inputs and one output at the block diagram of the adaptive FLC controller are addressed by the following equations at “k” sampling instant [91];

$$E(k) = \frac{[P(k) - P(k - 1)]}{[V(k) - V(k - 1)]} \quad (4)$$

$$\Delta E(k) = E(k) - E(k - 1) \quad (5)$$

$$D(k) = D(k - 1) + \Delta D(k) \quad (6)$$

Where;

- P(k) = Output power of PV system
- V(k) = Voltage at kth sampling time
- ΔD = Change in duty ratio cycle

The change of duty cycle ΔD acts as the Fuzzy logic controller's output where it is used to compute the DC-DC converter's real duty cycle (D(k) at the kth sampling and this will adjust according to the inputs applied the step size required to drive an operating point accordingly towards the MPP. E(k) is representing the error at the P-V curve slope.

Knowing that, the E(k) input of the FLC designate the operating point's position at a kth instance of time whether being located at the right or the left of the maximum power point (MPP) at the PV system's P-V curve.

The second input of the FLC denoted as $\Delta E(k)$ determines in which direction the operating point shall move; i.e., the moving direction of the operating point on the photovoltaic systems' P-V curve (left or right of the curve).

The Matlab Simulink was used to create and construct the membership functions of the first input of the FLC controller, the input error (E) as shown in Figure 9.

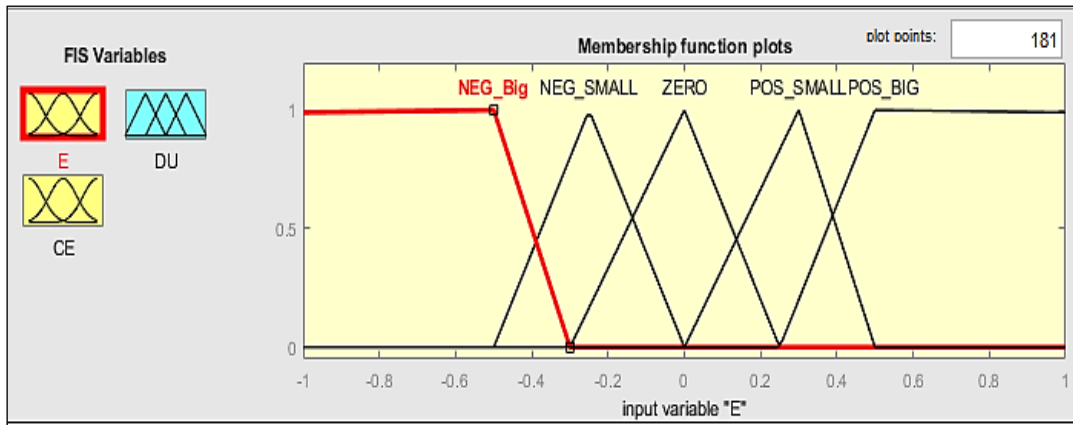


Figure 9. Construction of FLC input Error (E) membership functions

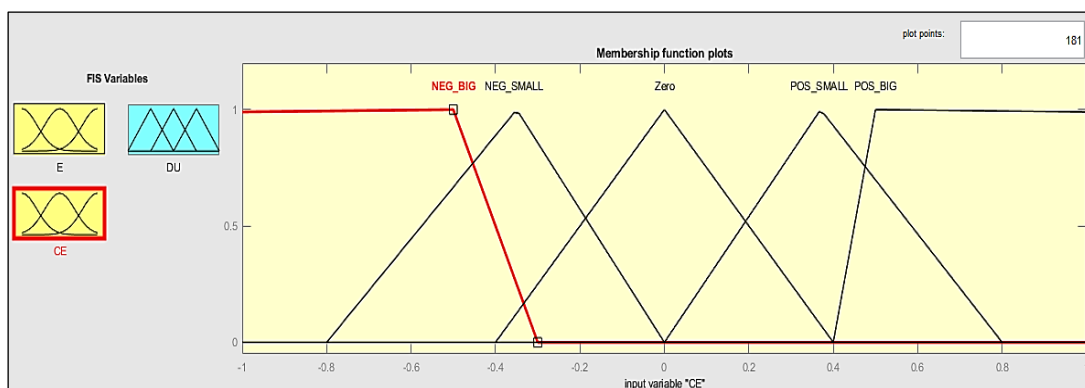


Figure 10. Construction of FLC input Change of Error (CE) MF

Similarly, Figure 10 depicts the change of error at a k^{th} sampling time.

Figure 11 depicts the duty ratio cycle output of the fuzzy logic which plays an essential part in determining the tuning of the applied step size perturbation to move the operating point on the photovoltaic system P-V curve towards the MPP.

By analyzing the changes in (V) and (P) of PV system, FLC will be capable of generating the duty cycle of the

DC-DC converter. Significantly, the duty cycle can range from 0 to 1. The FLC MPPT algorithm sends the signal representing the change in duty cycle to the pulse width modulation (PWM) module, which then switches the IGBT transistor to update automatically the converter's duty cycle. This dynamic adjustment has the advantage of extracting the maximum power (Pmax) from PV module.

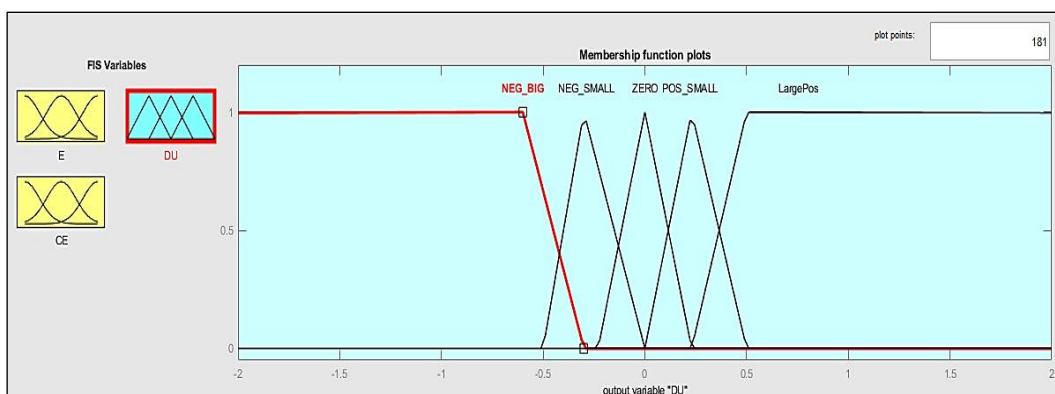


Figure 11. Construction of MF for duty ratio cycle (ΔD)

Note that the purpose of an FLC rule editor is to provide a software graphical user interface that enables the seamless creation or rules, tuning them and apply proper

adjustments and modify them according to the systems' parameters.

By simplifying the process of defining rules, MFs, and their relationships, and the linguistic variables, it facilitates for the designer the fine-tuning of the fuzzy logic controller rule base.

In Figure 12 we constructed the (rule editor) that consists of twenty-five rules.

A fragment of the twenty-five rules is shown using the fuzzy IF-THEN rules [91].

As mentioned earlier the FLC is consisting of five rule-based membership functions (MF); the universe of discourse is divided into five fuzzy sets to represent the five MF FLCs [91].

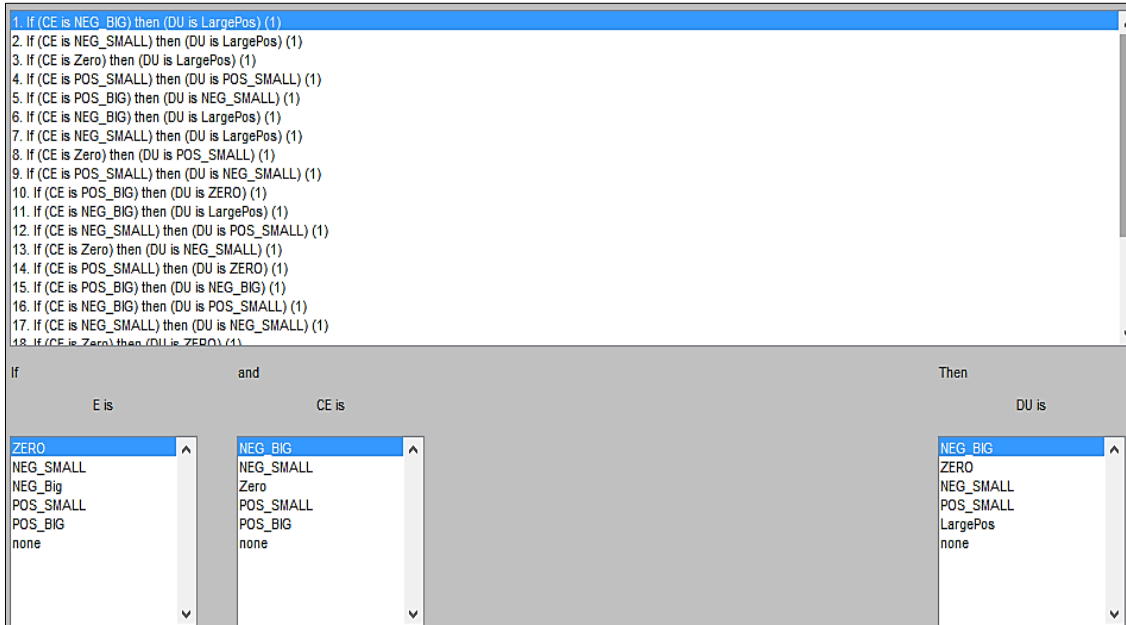


Figure 12. Rule Editor in Fuzzy logic tool box

6. SIMULATION AND DISCUSSION OF RESULTS

In this section a series of discussions will take place in regards to the findings and results obtained for the enhanced fuzzy logic-incremental conductance adaptive model.

Starting by the module manufacturing data, Figure 13 depicts the technical specifications of the tested solar panel; “Sharp-ND-62” parameters.

Module data	
Maximum Power (W)	61.992
Cells per module (Ncell)	18
Open circuit voltage Voc (V)	10.8
Short-circuit current Isc (A)	8
Voltage at maximum power point Vmp (V)	8.61
Current at maximum power point Imp (A)	7.2
Temperature coefficient of Voc (%/deg.C)	-0.3035
Temperature coefficient of Isc (%/deg.C)	0.0528

Figure 13. The manufacturer data sheet for Sharp solar

The general power, voltage and current curves are shown in Figure 14 for a 60 watts solar panel used in this research where the values from the technical graph shows the expected outputs of the power, voltage, and current of

this solar cell module and those can be verified with the obtained results through the simulations using variable step size adaptive INC based FLC.

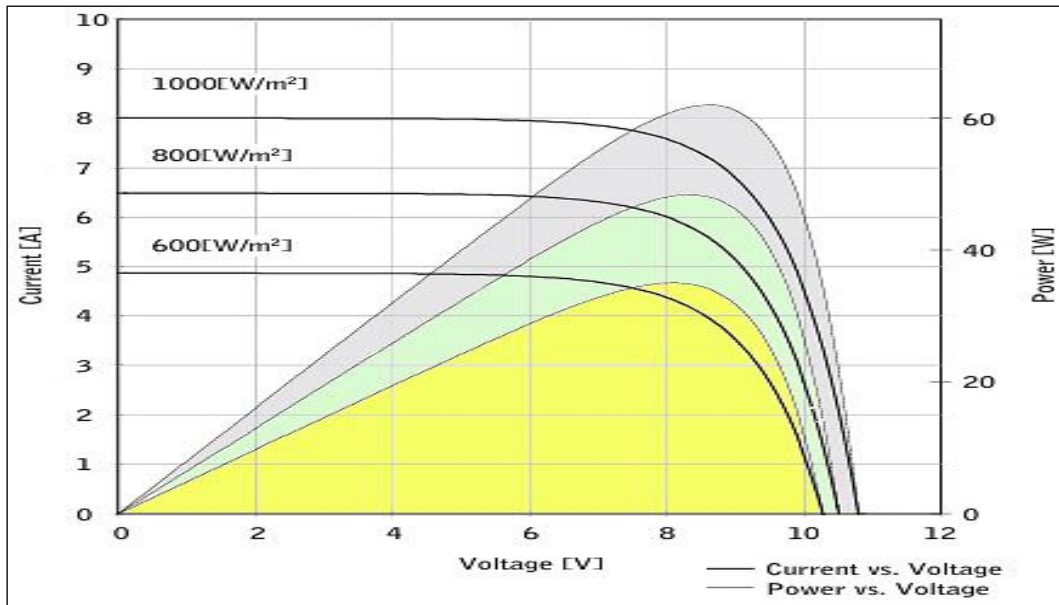


Figure 14. The Sharp-ND-62 graphical specifications

The output maximum power is set around 60 Watts when taken into consideration the standard test conditions (STC) with an irradiance of 1000w/m² and temperature at 25°C.

Our simulations of power, voltage and current are being tested at different set of irradiance levels ranging between 500, 800 1000 and again back to 500 w/m².

This represents how the optimal MPP varies in accordance with the variations in the irradiance at a constant test temperature condition.

The calculated power, voltage, and current through the simulation that we ran at the different ranges of irradiances (500, 800, and 1000 w/m²) after being fed with the appropriate inputs are shown in Figures 15, 16, and 17 respectively.

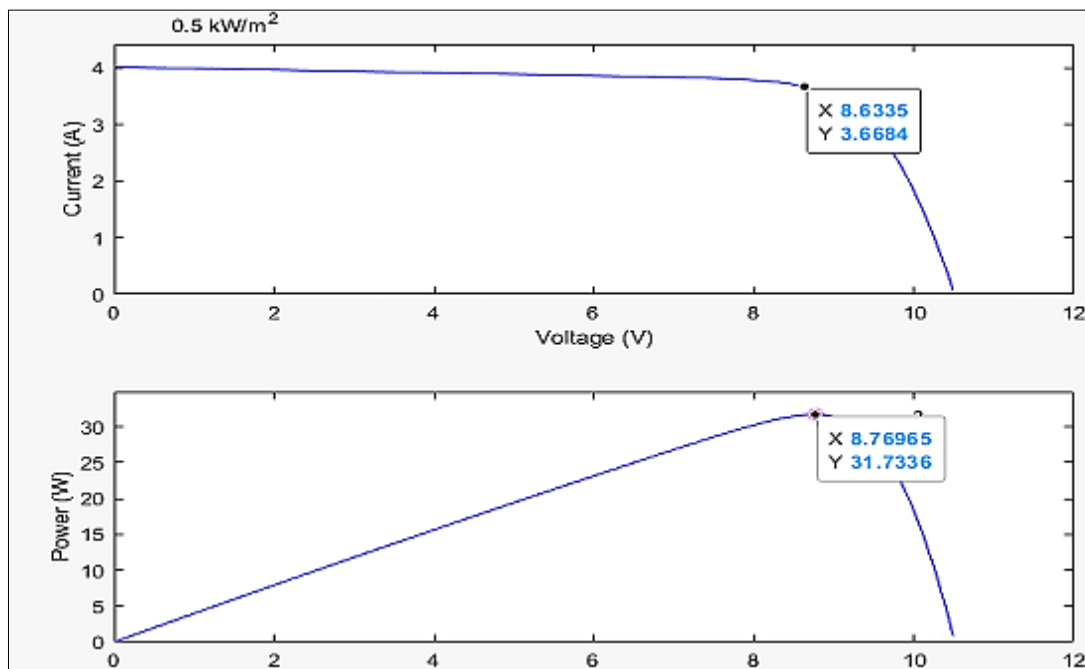


Figure 15. I-V and P-V curves at 500w/m²

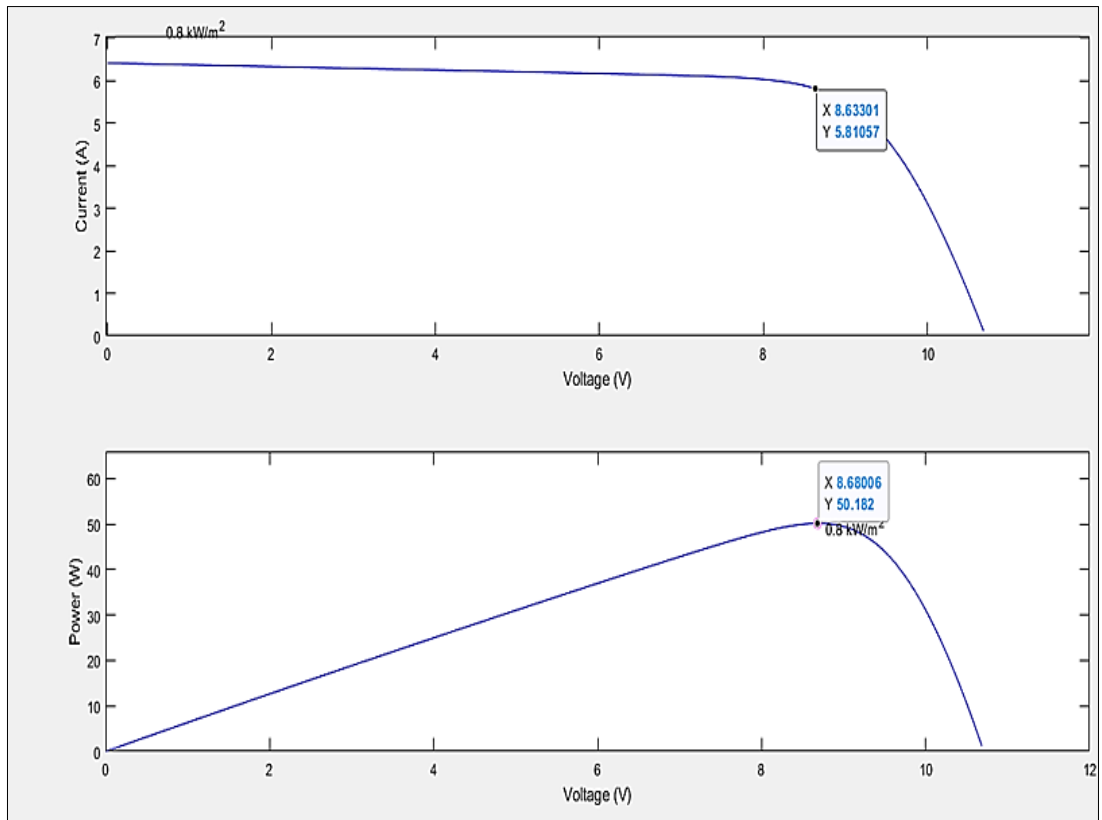


Figure 16. I-V and P-V curves at 800w/m²

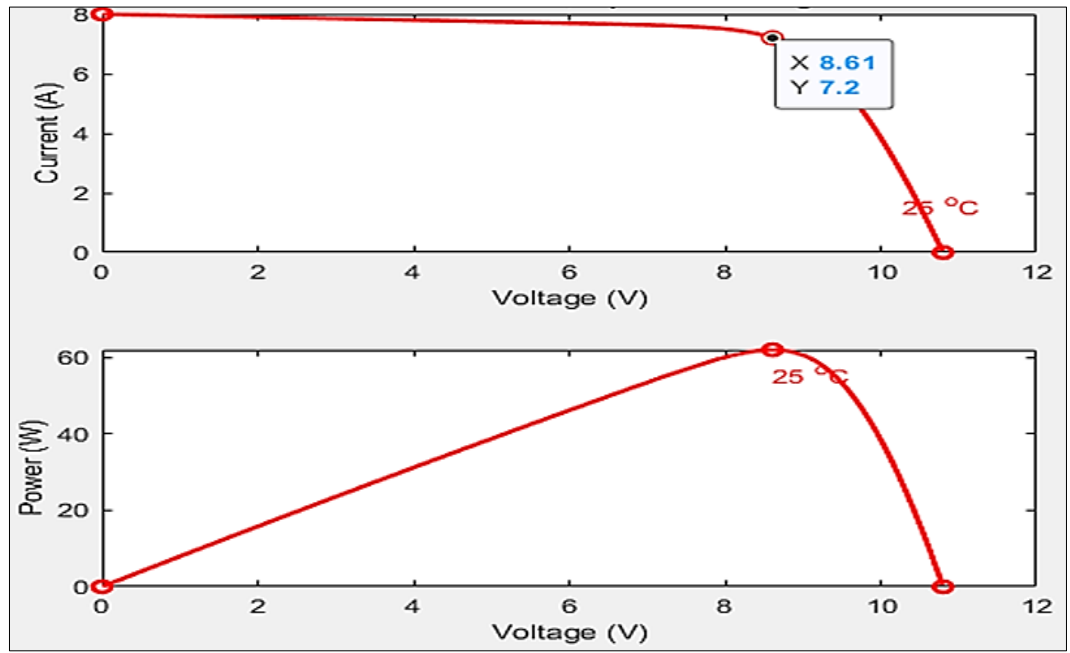


Figure 17. (I-V) and (P-V) curves at 1000w/m²

Table 2 concludes the results that shall be obtained after applying the adaptive fuzzy logic based incremental conductance with various step size.

The irradiance levels are shown in Figure 18 with respect to a sampling set of time.



Table 2. Effective measurement of P, V, and I at different irradiance levels

Irradiance (G)W/m ²	Power (P)	Voltage (V)	Current (I)
500	31.75	8.63	3.68
800	50.18	8.63	5.81
1000	62	8.61	7.2

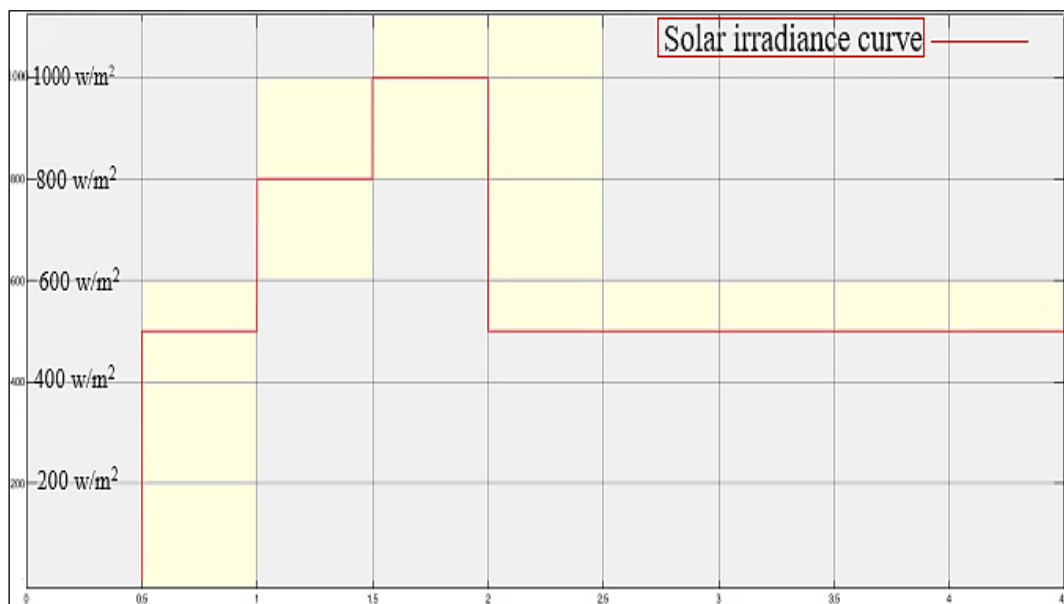
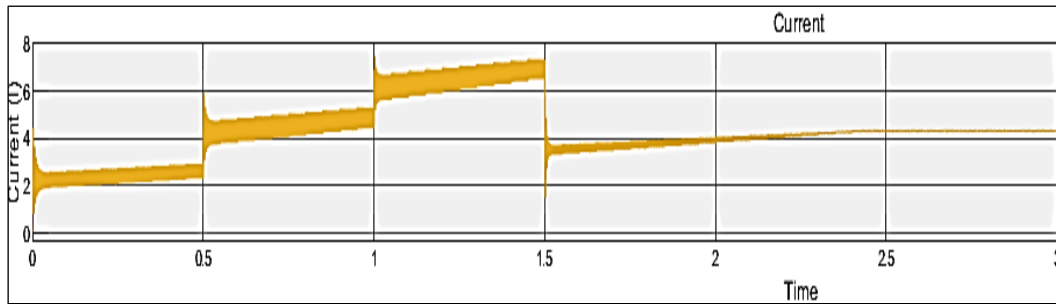


Figure 18. Step size of irradiances at different levels (0 to 1000 w/m²)

These varying steps are being tested against their effects on the Pmax, Vmax and Imax to verify the effective implementation of fuzzy logic control with incremental conductance in extracting the maximum power at different weather conditions.

As per Figure 19 the simulation output tests for the current (I) were based on adaptive fuzzy-incremental conductance variable step size model.

The results obtained were very close to those in table 1 (the theoretical calculations).

Figure 19. Simulation of current I at different irradiance levels (500, 800, and 1000 w/m²)

We analyzed the obtained current values versus the levels of applied irradiances (at the 500, 800 and 1000 w/m²).

Back to the 500 w/m² and by referring to table 1, the theoretical calculated current is 3.68A, and the simulated result was outputting a current of 3.3A.

At 800 w/m² the current calculated in table 1 is 5.81A and the obtained simulated result was 5.8A. At the

1000 w/m² Table 1 current was calculated 7.2A and the simulated output current at this irradiance level was close to 7.15A.

Figure 20 shows the voltage obtained at the different irradiances levels and those were tested for 500, 800, and 1000 w/m².

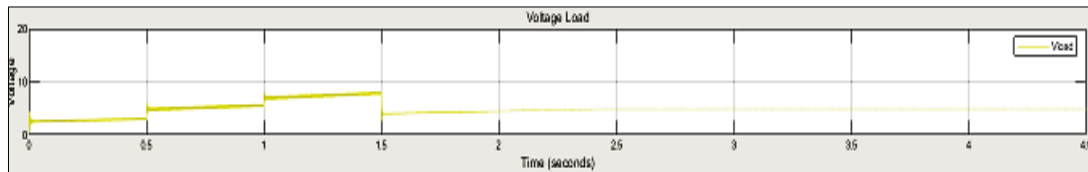


Figure 20. Simulated voltages at different irradiance levels

As per the voltage theoretical calculation versus results obtained from the simulated model, we may record the following;

At 500, 800, and 1000 w/m², the calculated voltages were 8.63V in accordance to the three different irradiances.

In Figure 20 the simulated results obtained were as follows; at the 500 w/m² the voltage was 7.8V, at 800 w/m² the voltage obtained was 8.61V, and at the standard test condition (1000 w/m²) the voltage obtained was 8.68V.

In the following discussion we will analyze the obtained

results with reference to the maximum power extracted from the PV module structure.

Before commencing the discussions, we will get a closer look at Figure 21 which is representing the measured values of power at the different irradiance levels.

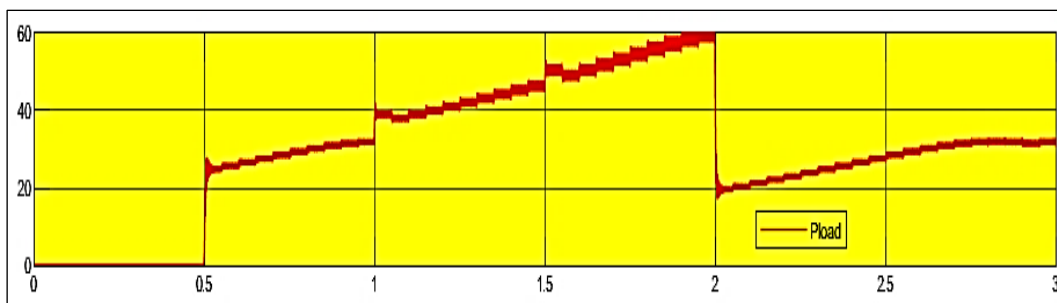


Figure 21. Maximum power extraction under varying irradiance levels

At the 500 w/m² irradiance level the calculated maximum power was 31.73 watts, and this value as it can be observed from Figure 21 the incremental conductance fuzzy logic with variable steps was able to reach that value at 0.76s, with a very satisfactory stable signal free of any oscillation, with a satisfactory climbing towards the maximum power point. At 800 w/m² the calculated maximum power was 50.18, and as compared to the one

obtained from the simulation, we can conclude that the simulated result was close to 49.56 at 1.23s. During the testing of the standard test condition (STC) which represents the temperature at 25° C, along with an irradiance of 1000 w/m², the calculated maximum power was 62 watts. The system was able to detect and reach that value at 1.82s time for the 1000 w/m² where the power



extraction reached 60 watts. Further we tested the system in a drastic shift from 1000 w/m² to 500w/m² to test the overall response in shifting at a sudden change in irradiance to verify the tracking of the P_{max} in accordance with the FLC controller’s efficiency versus such irradiance changes, and the result obtained was as follows; at 1.5s we decided to apply a sudden change in irradiance to verify how the system will behave and testing the time required to reach the Pmax while the system is tracking it.

As shown in Figure 20, at 1.82s the system tracked the maximum power for the value of 30.95w (calculated is 31.73 watts) within a 0.32 s time. This testing proved that the system was robust and efficient to work with any sudden changes in irradiances and getting the ability to reach and track the optimal power.

To conclude the above discussions and results, the below tables were used to compare the overall performance of the modified system in comparison of the calculated versus the simulation results of the maximum current (Imax), the maximum voltage (Vmax) and the maximum power (Pmax) of the photovoltaic system using a 62 watts sharp solar panels.

It is noted that the efficiency of the modified INC based variable step size FLC controller was able to accurately and in a faster response time to track the MPP at different irradiance levels. This conclude that the efficiency of the modified INC based FLC control was reaching more than 99.2 %.

In table 3, the maximum current (Imax) at the different applied irradiances was achieved with an average accuracy rate of more than 99.95%. As per table 4, the maximum voltage (Vmax) at the different applied irradiances was achieved with an average accuracy rate of more than

99.43 %, and through table 5, the maximum power (Pmax) at the different applied irradiances was achieved with an average accuracy rate of more than 99.12%.

In general, the simulation and experimental results specifies that the efficiency of the MPPT tracking system based FLC was achieved at a rate of more than 99.95% and further as per the simulation results the tracking response time and the convergence speed were at the minimal level where for instance to track the Pmax at;

500 w/m² it took 0.76 seconds, and at 800 w/m² the tracking time was 1.23 second and eventually at 1000 w/m² it took the modified MPPT system 1,82 seconds to reach Pmax of the solar panel system.

Table 3. Calculated VS simulated “Imax” at different irradiance levels

Irradiance	Calculated current value	Simulation current value
500 w/m ²	3.68 A	3.3 A
800 w/m ²	5.81 A	5.8 A
1000 w/m ²	7.2 A	7.15 A

Table 4. Calculated VS simulated “Vmax” at different irradiance levels

Irradiance	Calculated voltage value	Simulation voltage value
500 w/m ²	8.63 v	7.8 v

800 w/m ²	8.63 v	8.61 v
1000 w/m ²	8.7 v	8.68 v

Table 5. Calculated VS simulated “Pmax” at different irradiance levels

Irradiance	Calculated power value	Simulation power value
500 w/m ²	31.75 w	25.74 w
800 w/m ²	50.14 w	49.93 w
1000 w/m ²	62.64w	62.06 w

7. CONCLUSION

The conducted research has been applied in accordance of using an incremental conductance modified through an adaptive variable step size fuzzy logic controller. The design approach was to modify the INC MPPT algorithm to move from the conventional fixed step size perturbation into a variable step size modified MPPT using FLC by decrementing and incrementing of the DC-DC converter duty cycle. This has been implemented through a defined five membership functions (MFs) of the FLC inputs. Our applied testing was not only at the standard test conditions but went further to different irradiance levels to verify and stress out the modified system in testing its efficiency that reached in an overall bench mark efficiency of more than 99.5%. The tracking system was able to provide an overall high operational power efficiency (during the extraction of this power) along with a minimal/suppressed oscillation around the maximum power point, and a very fast response time in tracking the MPP at the different irradiances applied. The simulation tested many parameters associated with a PV module, ranging from the maximum voltage (Vmax), and maximum current (Imax), to tracking the maximum power (Pmax) at the varying tested irradiance levels. From the discussions conducted we can conclude that the results were well optimized to those calculated (theoretically) with respect to the tested parameters (Vmax, Imax, and Pmax) and the modified system was able to track the power at a fast response time as the irradiance was changing from one level to another, improved the DC output power, and minimized the convergence time for reaching the steady-state as switching through the various irradiance levels.

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